

P8.3 Consider temperature in the chip, neglecting heat conducted through the tool. Refer to Section 8.2.2 and Fig. P8.3.

(a) Chip width $b = 8 \text{ mm}$, $h_1 = 0.12 \text{ mm}$, $v = 3000 \text{ mm/sec}$, $K_s = 2000 \text{ N/mm}^2$, $L_c = 1.0 \text{ mm}$, $\phi = 30^\circ$, $\beta = 20^\circ$, $T_{room} = 20^\circ\text{C}$, $\Delta x = 0.002 \text{ mm}$, $\Delta y = 0.01 \text{ mm}$, $k = 40 \text{ N/(sec.}^\circ\text{C)}$, $(\rho c) = 3.6 \text{ N/(mm}^2 \cdot ^\circ\text{C)}$. Determine:

Shear-plane temperature: $v_s(\text{mm/sec})$, $F_s(\text{N})$, $P_s(\text{mW})$, $T_s(^\circ\text{C})$,

Friction power distribution: $F_f(\text{N})$, $v_c(\text{mm/sec})$, $P_f(\text{mW})$, $P_{max}(\text{mW})$:

Start of the potential computation:

Determine $T_{1,1}$, $T_{2,1}$, $T_{3,1}$, $T_{1,2}$, $T_{2,2}$, $T_{3,2}$

(b) Chip width $b = 10 \text{ mm}$, $h_1 = 0.15 \text{ mm}$, $v = 2500 \text{ mm/sec}$, $K_s = 2000 \text{ N/mm}^2$, $L_c = 1.0 \text{ mm}$, $\phi = 30^\circ$, $\beta = 20^\circ$, $T_{room} = 20^\circ\text{C}$, $\Delta x = 0.002 \text{ mm}$, $\Delta y = 0.01 \text{ mm}$, $k = 40 \text{ N/(sec.}^\circ\text{C)}$, $(\rho c) = 3.6 \text{ N/(mm}^2 \cdot ^\circ\text{C)}$.

(c) $b = 10 \text{ mm}$, $h_1 = 0.1 \text{ mm}$, $h_2 = 0.2 \text{ mm}$, $\Delta x = 0.002 \text{ mm}$, $\Delta y = 0.01 \text{ mm}$, $K_s = 1800 \text{ N/mm}^2$, $v = 2500 \text{ mm/sec}$, $k = 24.5 \text{ N/(sec.}^\circ\text{C)}$, $(\rho c) = 3.5 \text{ N/(mm}^2 \cdot ^\circ\text{C)}$, $\phi = 26.57^\circ$, $\beta = 20^\circ$, $T_{room} = 20^\circ\text{C}$.

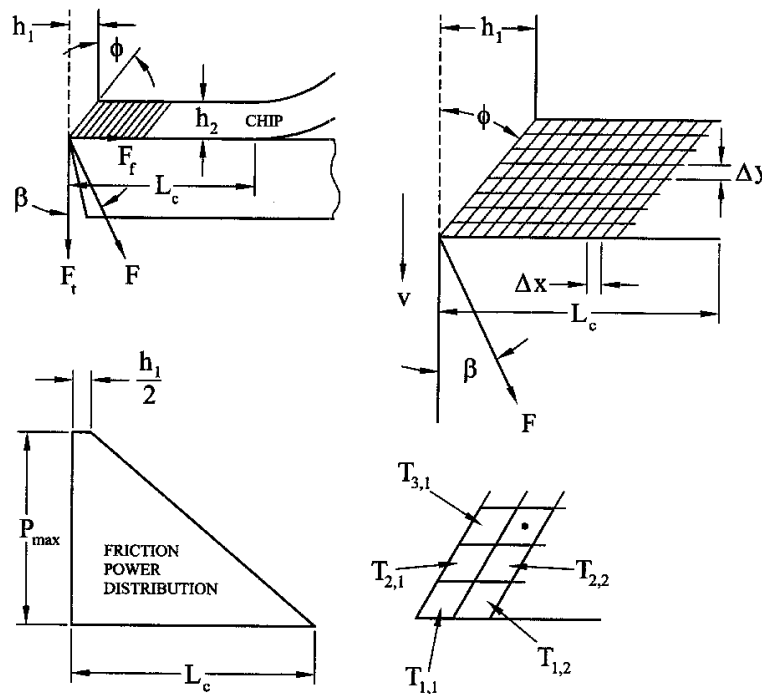
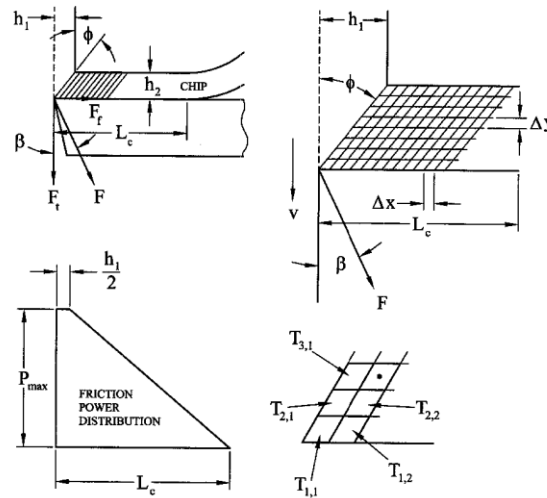


Figure P8.3

P8.4 Consider temperature in the chip; neglect heat conducted through the tool. Refer to Section 8.2.2 and Fig. P8.3. Machining steel 1035, $k = 43 \text{ N}/(\text{sec} \cdot ^\circ\text{C})$, $\alpha = 12 \text{ mm}^2/\text{sec}$, $(\rho c) = 3.7 \text{ N}/(\text{mm}^2 \cdot ^\circ\text{C})$, $h_1 = 0.2 \text{ mm}$, $b = 10 \text{ mm}$, $L_c = 0.8 \text{ mm}$, $v_c = 1.5(\text{m}/\text{sec})$, $\Delta x = 0.0025 \text{ mm}$, $\Delta y = 0.02 \text{ mm}$, $\beta = 20^\circ$, $\phi = 25^\circ$.



The following values have been precomputed: Shear-plane temperature $T_s = 510^\circ\text{C}$, friction power $P_f = 2.07 \times 10^6 \text{ N} \cdot \text{mm}/\text{s} (\text{mW})$.

- (a) Determine P_{max} .
- (b) Determine the initial temperatures in the thermal field: $T_{1,1}, T_{2,1}, T_{3,1}, T_{1,2}, T_{2,2}$.

P8.5 Consider temperatures in the chip; neglect heat through the tool. Refer to Section 8.2.2 and Fig. P8.5 and P8.10. Cutting steel $K_s = 2000 \text{ N}/\text{mm}^2$, $(\rho c) = 3.7 \text{ N}/(\text{mm}^2 \cdot ^\circ\text{C})$, $h_1 = 0.25 \text{ mm}$, $b = 8 \text{ mm}$, $\beta = 25^\circ$, $\phi = 30^\circ$, $\alpha = 0^\circ$, $v = 3 \text{ m}/\text{sec}$. Determine cutting force $F(\text{N})$, shearing force $F_s(\text{N})$, shearing velocity $v_s(\text{mm}/\text{sec})$, shearing power $P_s(\text{N} \cdot \text{mm}/\text{s})$, and shear-plane temperature $T_s(^\circ\text{C})$, assuming $T_{room} = 20^\circ\text{C}$. Thermal diffusivity $\alpha = 12 \text{ mm}^2/\text{sec}$. Determine chip velocity v_c , friction force F_f , and friction power $P_f(\text{N} \cdot \text{mm}/\text{s})$. Element dimensions: $\Delta x = 0.0025 \text{ mm}$, $\Delta y = 0.022 \text{ mm}$. Determine time step Δt . In the course of computation, we find: $T_{1,165} = 779.2^\circ\text{C}$, $T_{2,165} = 706.0^\circ\text{C}$, $T_{3,165} = 670.1^\circ\text{C}$, and $T_{1,166} = 781.0^\circ\text{C}$. Determine $T_{2,166}$.

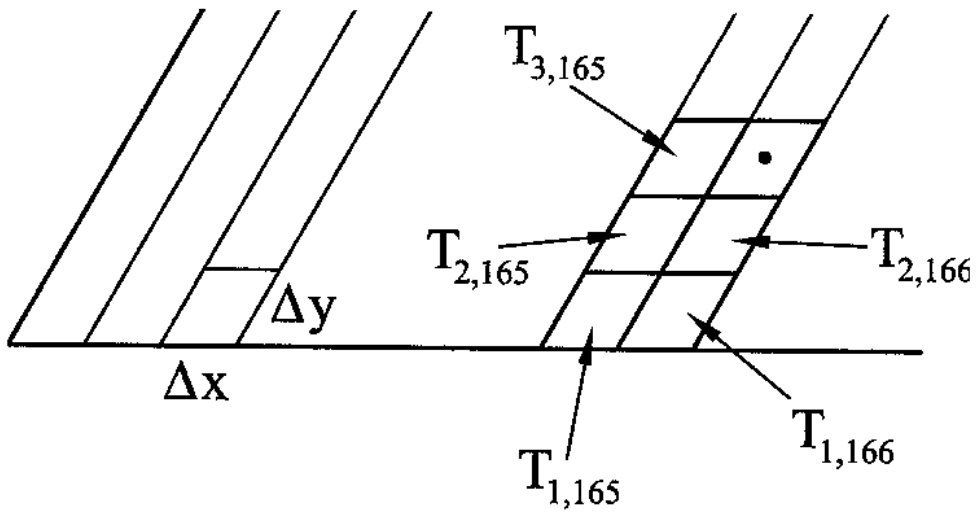


Figure P8.5