



Finite Element Method Integral Formulation



Some Mathematical Concepts

Simply connected domain: If any two points of the domain can be Joint by a line lying entirely within the domain

Class of a domain: A function of several variables is said to be of Class $C^m(\Omega)$ in a domain if all its partial derivatives up to and including the m th order exist and are continuous in Ω

$C^0 \rightarrow F$ is continuous (i.e. $\partial f / \partial x$, $\partial f / \partial y$ exist but may not be continuous.)

Boundary Value Problems: A differential equation (DE) is said to be a BVP if the dependent variable and possibly its derivatives are required to take specified values on the boundary.

Example:
$$-\frac{d}{dx}\left(a \frac{du}{dx}\right) = f \quad 0 < x < 1, \quad u(0) = d_0, \quad \left(x \frac{du}{dx}\right)_{x=1} = g_0$$



Some Mathematical Concepts

Initial Value Problem: An IVP is one in which the dependent variable and possibly its derivatives are specified initially at $t = 0$

Example:
$$\rho \frac{d^2 u}{dt^2} + au = f \quad 0 < t \leq t_0, \quad u(0) = u_0, \quad \left(\frac{du}{dt} \right)_{t=0} = v_0$$

Initial and Boundary Value Problem:

Example:
$$-\frac{\partial}{\partial x} \left(a \frac{\partial u}{\partial x} \right) + \rho \frac{\partial u}{\partial t} = f(x, t) \quad \text{for } 0 < x < 1 \text{ and } 0 < t \leq t_0$$

$$u(0, t) = d_0(t), \quad \left(a \frac{\partial u}{\partial x} \right)_{x=1} = g_0(t), \quad u(x, 0) = u_0(x)$$

Eigenvalue Problem: the problem of determining value λ of such that

Example:
$$-\frac{d}{dx} \left(a \frac{du}{dx} \right) = \lambda u \quad 0 < x < 1$$

$$u(0) = 0, \quad \left(\frac{du}{dx} \right)_{x=1} = 0$$

λ Eigenvalue
 u Eigenfunction



Some Mathematical Concepts

Integration-by-Part Formula:

First

$$\frac{d}{dx}(wv) = \frac{dw}{dx}v + w\frac{dv}{dx} \Rightarrow \int_a^b w \frac{dv}{dx} dx = -\int_a^b v \frac{dw}{dx} dx + w(b)v(b) - w(a)v(a)$$

Next

$$\int_a^b w \frac{d^2u}{dx^2} dx = -\int_a^b \frac{du}{dx} \frac{dw}{dx} dx + w(b) \frac{du}{dx}(b) - w(a) \frac{du}{dx}(a)$$

Similarly

$$\int_a^b v \frac{d^4w}{dx^4} dx = \int_a^b \frac{d^2w}{dx^2} \frac{d^2v}{dx^2} dx + \frac{d^2w}{dx^2}(a) \frac{dv}{dx}(a) - \frac{d^2w}{dx^2}(b) \frac{dv}{dx}(b) + v(b) \frac{d^3w}{dx^3}(b) - v(a) \frac{d^3w}{dx^3}(a)$$



Some Mathematical Concepts

Gradient Theorem

$$\int_{\Omega} \text{grad } F \, dx dy = \int_{\Omega} \nabla F \, dx dy = \oint_{\Gamma} \hat{n} F \, ds$$

But

$$\nabla F = \frac{\partial F}{\partial x} i + \frac{\partial F}{\partial y} j, \quad \hat{n} = n_x i + n_y j$$

Thus

$$\int_{\Omega} \left(\frac{\partial F}{\partial x} i + \frac{\partial F}{\partial y} j \right) dx dy = \oint_{\Gamma} (n_x i + n_y j) F \, ds$$

or

$$\int_{\Omega} \left(\frac{\partial F}{\partial x} \right) dx dy = \oint_{\Gamma} F n_x \, ds$$

$$\int_{\Omega} \left(\frac{\partial F}{\partial y} \right) dx dy = \oint_{\Gamma} F n_y \, ds$$



Some Mathematical Concepts

Divergence Theorem

$$\int_{\Omega} \operatorname{div} G \, dx dy = \int_{\Omega} \nabla \cdot G \, dx dy = \oint_{\Gamma} \hat{n} \cdot G ds$$

$$\int_{\Omega} \left(\frac{\partial G_x}{\partial x} + \frac{\partial G_y}{\partial y} \right) dx dy = \oint_{\Gamma} (n_x G_x + n_y G_y) ds$$

Using gradient and divergence theorem, the following relations can be derived! (Exercise)

$$\int_{\Omega} (\nabla G) w \, dx dy = - \int_{\Omega} (\nabla w) G \, dx dy + \oint_{\Gamma} \hat{n} w G ds \quad (*) \quad \text{and}$$

$$- \int_{\Omega} (\nabla^2 G) w \, dx dy = \int_{\Omega} (\nabla w) \cdot (\nabla G) \, dx dy - \oint_{\Gamma} \frac{\partial G}{\partial n} w ds$$



Some Mathematical Concepts

The components of equation (*) are:

$$\int_{\Omega} \frac{\partial G}{\partial x} w dx dy = - \int_{\Omega} \frac{\partial w}{\partial x} G dx dy + \oint_{\Gamma} n_x w G ds$$

$$\int_{\Omega} \frac{\partial G}{\partial y} w dx dy = - \int_{\Omega} \frac{\partial w}{\partial y} G dx dy + \oint_{\Gamma} n_y w G ds$$



Some Mathematical Concepts

Functionals

An integral in the form of

$$I(u) = \int_a^b F(x, u, u') dx, \quad u = u(x), \quad u' = \frac{du}{dx}$$

where integrand $F(x, u, u')$ is a given function of arguments x, u, u' is called a **functional** (a function of function) .

A functional is said to be **linear** if and only if:

$$I(\alpha u + \beta v) = \alpha I(u) + \beta I(v) \quad \alpha, \beta \text{ are scalars}$$

A functional $B(u, v)$ is said to be **bilinear** if it is linear in each of its arguments

$$B(\alpha u_1 + \beta u_2, v) = \alpha B(u_1, v) + \beta B(u_2, v) \quad \text{Linearity in the first argument}$$

$$B(u, \alpha v_1 + \beta v_2) = \alpha B(u, v_1) + \beta B(u, v_2) \quad \text{Linearity in the second argument}$$



Some Mathematical Concepts

Functionals

A bilinear form $B(u, v)$ is *symmetric* in its arguments if

$$B(u, v) = B(v, u)$$

Example of linear functional is

$$I(v) = \int_0^L v f dx + \frac{dv}{dx}(L) M_0$$

Example of bilinear functional is

$$B(v, w) = \int_0^L a \frac{dv}{dx} \frac{dw}{dx} dx$$



Some Mathematical Concepts

4.4.1 The Variational Operator

The delta operator δ used in conjunction with virtual quantities has special importance in variational methods. The operator is called the *variational operator* because it is used to denote a variation (or change) in a given quantity. In this section, we discuss certain operational properties of δ and elements of variational calculus. Using these tools, we can study the energy and variational principles of general problems.

Let $u = u(x)$ be the true configuration (i.e., the one corresponding to equilibrium) of a given mechanical system, and suppose that $u = \hat{u}$ on boundary S_1 of the total boundary S . Then an admissible configuration is of the form

$$\bar{u} = u + \alpha v \quad (4.62)$$

everywhere in the body, where v is an arbitrary function that satisfies the homogeneous geometric boundary condition of the system

$$v = 0 \quad \text{on } S_1. \quad (4.63)$$

Some Mathematical Concepts

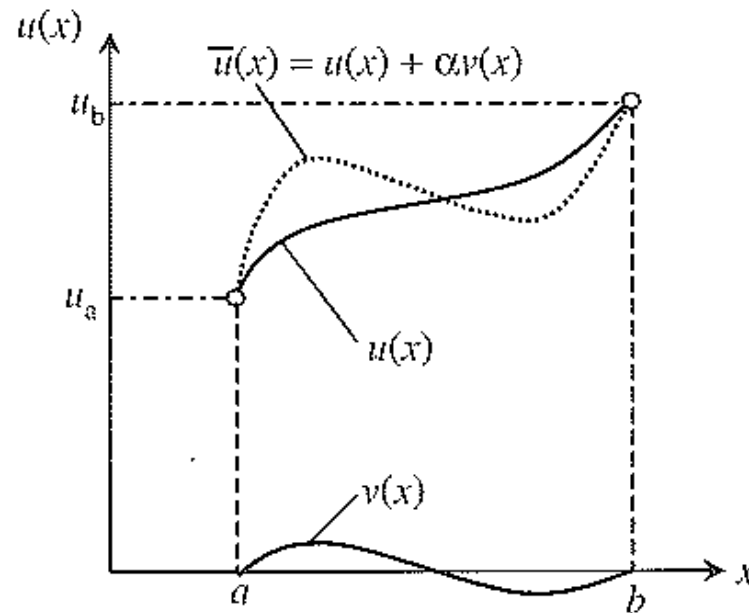


Figure 4.13 The variations of $u(x)$.

the space of admissible variations, as already mentioned. Figure 4.13 shows a typical competing function $\bar{u}(x) = u(x) + \alpha v(x)$ and a typical admissible variation $v(x)$.



Some Mathematical Concepts

Here αv is a variation of the given configuration u . It should be understood that *the variations are small enough* (i.e., α is small) *not to disturb the equilibrium of the system, and the variation is consistent with the geometric constraint of the system.* Equation (4.62) defines a set of varied configurations; an infinite number of configurations \bar{u} can be generated for a fixed v by assigning values to α . All of these configurations satisfy the specified geometric boundary conditions on boundary S_1 , and therefore they constitute the set of admissible configurations. For any v , all configurations reduce to the actual one when α is zero. Therefore for any *fixed* x , αv can be viewed as a change or *variation* in the actual configuration u . This variation is often denoted by δu :

$$\delta u = \alpha v, \quad \delta \left(\frac{du}{dx} \right) = \alpha \left(\frac{dv}{dx} \right) = \frac{d(\alpha v)}{dx} = \frac{d\delta u}{dx}, \quad (4.64)$$

and δu is called the *first variation* of u .



Some Mathematical Concepts

Next, consider a function of the dependent variable u and its derivative $u' \equiv du/dx$:

$$F = F(x, u, u'). \quad (4.65)$$

For fixed x , the change in F associated with a variation in u (and hence u') is

$$\begin{aligned} \Delta F &= F(x, u + \alpha v, u' + \alpha v') - F(x, u, u') \\ &= F(x, u, u') + \frac{\partial F}{\partial u} \alpha v + \frac{\partial F}{\partial u'} \alpha v' \\ &\quad + \frac{(\alpha v)^2}{2!} \frac{\partial^2 F}{\partial u^2} + \frac{2(\alpha v)(\alpha v')}{2!} \frac{\partial^2 F}{\partial u \partial u'} + \dots - F(x, u, u') \\ &= \frac{\partial F}{\partial u} \alpha v + \frac{\partial F}{\partial u'} \alpha v' + O(\alpha^2), \end{aligned} \quad (4.66)$$



Some Mathematical Concepts

where $O(\alpha^2)$ denotes terms of order α^2 and higher. The first total variation of $F(x, u, u')$ is defined by

$$\begin{aligned}\delta F &= \alpha \left[\lim_{\alpha \rightarrow 0} \frac{\Delta F}{\alpha} \right] \\ &= \alpha \left(\frac{\partial F}{\partial u} v + \frac{\partial F}{\partial u'} v' \right) \\ &= \frac{\partial F}{\partial u} \alpha v + \frac{\partial F}{\partial u'} \alpha v' \\ &= \frac{\partial F}{\partial u} \delta u + \frac{\partial F}{\partial u'} \delta u'.\end{aligned}\tag{4.67a}$$



Some Mathematical Concepts

Alternatively, the first variation may be defined as

$$\begin{aligned}\delta F &= \alpha \left[\frac{dF(u + \alpha v, u' + \alpha v')}{d\alpha} \right]_{\alpha=0} \\ &= \frac{\partial F}{\partial u} \alpha v + \frac{\partial F}{\partial u'} \alpha v' \\ &= \frac{\partial F}{\partial u} \delta u + \frac{\partial F}{\partial u'} \delta u'.\end{aligned}\tag{4.67b}$$

There is an analogy between the first variation of F and the total differential of F . The total differential of F is

$$dF = \frac{\partial F}{\partial x} dx + \frac{\partial F}{\partial u} du + \frac{\partial F}{\partial u'} du'. \tag{4.68}$$



Some Mathematical Concepts

If $G = G(u, v, w)$ is a function of several dependent variables (and possibly their derivatives), the total variation is the sum of partial variations:

$$\delta G = \delta_u G + \delta_v G + \delta_w G, \quad (4.70)$$

where, for example, δ_u denotes the partial variation with respect to u . The variational operator can be interchanged with differential and integral operators:

$$(1) \quad \delta \left(\frac{du}{dx} \right) = \alpha \frac{dv}{dx} = \frac{d}{dx}(\alpha v) = \frac{d}{dx}(\delta u).$$

$$(2) \quad \delta \left(\int_0^a u \, dx \right) = \alpha \int_0^a v \, dx = \int_0^a \alpha v \, dx = \int_0^a \delta u \, dx. \quad (4.71)$$



Some Mathematical Concepts

The Variational Symbol

Consider the function $F = F(x, u, u')$ for fixed value of x , F only depends on u, u'

The change αv in u , where α is constant and v is a function, is called variation of u and denoted by:

$$\text{Variational Symbol} \longrightarrow \delta u = \alpha v$$

In analogy with the total differential of a function

$$\delta F = \frac{\partial F}{\partial u} \delta u + \frac{\partial F}{\partial u'} \delta u'$$

Note that

$$dF = \frac{\partial F}{\partial x} dx + \frac{\partial F}{\partial u} du + \frac{\partial F}{\partial u'} du'$$



Some Mathematical Concepts

The Variational Symbol

$$\text{Also } \delta(F_1 \pm F_2) = \delta F_1 \pm \delta F_2$$

$$\delta(F_1 F_2) = F_2 \delta F_1 + F_1 \delta F_2$$

$$\delta\left(\frac{F_1}{F_2}\right) = \frac{F_2 \delta F_1 - F_1 \delta F_2}{F_2^2}$$

$$\delta[(F_1)^n] = n(F_1)^{n-1} \delta F_1$$

Furthermore

$$\frac{d}{dx}(\delta u) = \frac{d}{dx}(\alpha v) = \alpha \frac{dv}{dx} = \alpha v' = \delta u' = \delta\left(\frac{du}{dx}\right)$$

$$\delta \int_a^b u(x) dx = \int_a^b \delta u(x) dx$$



Weak Formulation of BVP

Weighted – integral and weak formulation

Consider the following DE

$$-\frac{d}{dx} \left[a(x) \frac{du}{dx} \right] = q(x) \quad 0 < x < L$$

$$u(0) = u_0, \quad \left(a \frac{du}{dx} \right)_{x=L} = Q_0$$

Transverse deflection of a cable
Axial deformation of a bar
Heat transfer
Flow through pipes
Flow through porous media
Electrostatics



Weak Formulation of BVP

There are 3 steps in the development of a weak form, if exists, of any DE.

STEP 1:

Move all expression in DE to one side, multiply by w (weight function) and integral over the domain.

$$\int_0^L w \left[-\frac{d}{dx} \left(a \frac{du}{dx} \right) - q \right] dx = 0 \quad (+)$$

Weighted-integral or *weighted-residual*

$$u = U_N = \sum_{j=1}^N c_j \phi_j + \phi_0 \quad N \text{ linearly independent equation for } w \text{ and obtain } N \text{ equation for } c_1, \dots, c_N$$



Weak Formulation of BVP

STEP 2

- 1-The integral (+) allows to obtain N independent equations
- 2- The approximation function, ϕ , should be differentiable as many times as called for the original DE.
- 3- The approximation function should satisfy the BCs.
- 4- If the differentiation is distributed between w and ϕ then the resulting integral form has weaker continuity conditions. Such a weighted-integral statement is called **weak form**.

The weak form formulation has two main characteristics:

- requires weaker continuity on the dependent variable and often results in a symmetric set of algebraic equations.
- The **natural BCs** are included in the weak form, and therefore the approximation function is required to satisfy only the **essential BCs**.



Weak Formulation of BVP

Returning to our example:

$$\int_0^L \left\{ w \left[-\frac{d}{dx} \left(a \frac{du}{dx} \right) \right] - wq \right\} dx = 0 \Rightarrow \int_0^L \left(\frac{dw}{dx} a \frac{du}{dx} - wq \right) dx - \left[wa \frac{du}{dx} \right]_0^L = 0$$

Secondary Variable (SV):

Coefficient of weight function and its derivatives

$$Q = \left(a \frac{du}{dx} \right) n_x \quad \longrightarrow \quad \text{Natural Boundary Conditions (NBC)}$$

Primary Variable (PV): The dependent variable of the problem

$$u \quad \longrightarrow \quad \text{Essential Boundary Conditions (EBC)}$$



Weak Formulation of BVP

$$\int_0^L \left(\frac{dw}{dx} a \frac{du}{dx} - wq \right) dx - \left[wa \frac{du}{dx} \right]_0^L = 0$$

$$\int_0^L \left(\frac{dw}{dx} a \frac{du}{dx} - wq \right) dx - \left[wa \frac{du}{dx} n_x \right]_{x=0} - \left[wa \frac{du}{dx} n_x \right]_{x=L} = 0$$

$$\int_0^L \left(\frac{dw}{dx} a \frac{du}{dx} - wq \right) dx - (wQ)_0 - (wQ)_L = 0$$

Note that

$$n_x = -1 \quad x = 0$$

$$n_x = 1 \quad x = L$$



Weak Formulation of BVP

STEP 3:

The last step is to impose the actual BCs of the problem w has to satisfy the *homogeneous form* of specified EBC.

In weak formulation w has the meaning of a virtual change in PV. If PV is specified at a point, its variation is zero.

$$u(0) = u_0 \Rightarrow w(0) = 0$$

$$\left(a \frac{du}{dx} n_x \right)_{x=L} = \left(a \frac{du}{dx} \right)_{x=L} = Q_0 \text{ NBC}$$

Thus

$$\int_0^L \left(\frac{dw}{dx} a \frac{du}{dx} - wq \right) dx - \left[wa \frac{du}{dx} n_x \right]_{x=0} - \left[wa \frac{du}{dx} n_x \right]_{x=L} = 0$$

$$\int_0^L \left(\frac{dw}{dx} a \frac{du}{dx} - wq \right) dx - w(L)Q_0 = 0$$



Linear and Bilinear Forms

$$\underbrace{\int_0^L \left(\frac{dw}{dx} a \frac{du}{dx} \right) dx}_{B(w, u)} - \underbrace{\int_0^L w q dx - w(L) Q_0}_{l(w)} = 0 \quad \Rightarrow \quad B(w, u) - l(w) = 0$$

$B(w, u)$ Bilinear and symmetric in w and u

$l(w)$ Linear

Therefore, problem associated with the DE can be stated as one of finding the solution u such that $B(w, u) = l(w)$

holds for any w satisfies the homogeneous form of the EBC and continuity condition implied by the weak form



Linear and Bilinear Forms

Assume

$$u = u^* + w \quad \longrightarrow$$

Satisfy the homogeneous Form of EBC

Variational solution
Satisfy EBC

Actual solution
Satisfy EBC+NBC

Looking at the definition of the variational symbol, w is the variation of the solution, i.e.

$$w = \delta u$$

Then $B(w, u) = l(w) \Rightarrow B(\delta u, u) = l(\delta u)$ (#)

$$B(\delta u, u) = \int_0^L a \frac{d\delta u}{dx} \frac{du}{dx} dx = \delta \int_0^L \frac{a}{2} \left[\left(\frac{du}{dx} \right)^2 \right] dx = \frac{1}{2} \delta \int_0^L a \frac{du}{dx} \frac{du}{dx} dx = \frac{1}{2} \delta [B(u, u)]$$

$$l(\delta u) = \int_0^L \delta u q dx + \delta u(L) Q_0 = \delta \left[\int_0^L u q dx + u(L) Q_0 \right] = \delta [l(u)]$$



Linear and Bilinear Forms

Substituting in (#), we have:

$$B(\delta u, u) - l(\delta u) = 0 \Rightarrow \delta \left[\frac{1}{2} B(u, u) - l(u) \right] = 0 \Rightarrow \delta I(u) = 0$$

$$I(u) = \frac{1}{2} B(u, u) - l(u) \quad (\#\#)$$

In general, the relation $B(\delta u, u) = \frac{1}{2} \delta B(u, u)$ holds only if

$B(w, u)$ is bilinear and symmetric and $l(w)$ is linear

If $B(w, u)$ is not linear but symmetric the functional $I(u)$ can be derived but not from (##). (see Oden & Reddy, 1976, Reddy 1986)



Linear and Bilinear Forms

Equation $\delta I(u) = 0$ represents the necessary condition for the functional $I(u)$ to have an extremum value. For solid mechanics, $I(u)$ represents the total potential energy functional and the statement of the *total potential energy principle*.

Of all admissible function u , that which makes the total potential energy $I(u)$ a minimum also satisfies the differential equation and natural boundary condition in (+).



Some Examples

Example 1

Consider the following *DE* which arise in the study of the deflection of a cable or heat transfer in a fin (when $c = 0$).

$$-\frac{d}{dx} \left(a \frac{du}{dx} \right) - cu + x^2 = 0 \quad \text{for } 0 < x < 1$$

$$u(0) = 0, \quad \left(a \frac{du}{dx} \right)_{x=1} = 1$$

Step 1

$$\int_0^1 w \left[-\frac{d}{dx} \left(a \frac{du}{dx} \right) - cu + x^2 \right] dx = 0$$

Step 2

$$\int_0^1 \left(a \frac{dw}{dx} \frac{du}{dx} - cuw + wx^2 \right) dx - \left(wa \frac{du}{dx} \right)_0^1 = 0 \quad \Rightarrow \quad \begin{array}{ll} u(0) = 0 & EBC \\ \left(a \frac{du}{dx} \right)_{x=1} = 1 & NBC \\ w(0) = 0 & \end{array}$$



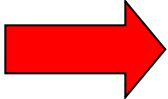
Some Examples

Example 1

Step 3
$$\int_0^1 \left(a \frac{dw}{dx} \frac{du}{dx} - cuw \right) dx + \int_0^1 wx^2 dx - w(1) = 0$$

or
$$B(w, u) = \int_0^1 \left(a \frac{dw}{dx} \frac{du}{dx} - cuw \right) dx$$

$$l(w) = - \int_0^1 wx^2 dx + w(1)$$


$$B(w, u) - l(w) = 0$$

B is bilinear and symmetric and l is linear! (prove)

Thus we can compute the quadratic functional form

$$I(u) = \frac{1}{2} \int_0^1 \left(a \left(\frac{du}{dx} \right)^2 - cu^2 + 2ux^2 \right) dx - u(1)$$



Some Examples

Example 2

Consider the following fourth-order *DE* (elastic bending of beam)

$$\frac{d^2}{dx^2} \left(b \frac{d^2 w}{dx^2} \right) - f(x) = 0 \quad \text{for } 0 < x < L$$

$$w(0) = \frac{dw(0)}{dx} = 0, \quad \left(b \frac{d^2 w}{dx^2} \right)_{x=L} = M_0, \quad \frac{d}{dx} \left(b \frac{d^2 w}{dx^2} \right)_{x=L} = 0$$

Step 1

$$\int_0^L v \left[\frac{d^2}{dx^2} \left(b \frac{d^2 w}{dx^2} \right) - f \right] dx = 0$$

Step 2

$$\int_0^L \left[\left(-\frac{dv}{dx} \right) \frac{d}{dx} \left(b \frac{d^2 w}{dx^2} \right) - vf \right] dx + \left[v \frac{d}{dx} \left(b \frac{d^2 w}{dx^2} \right) \right]_0^L = 0$$

Some Examples

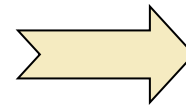
Example 2

$$\int_0^L \left(b \frac{d^2 v}{dx^2} \frac{d^2 w}{dx^2} - v f \right) dx + \left[v \frac{d}{dx} \left(b \frac{d^2 w}{dx^2} \right) - \frac{dv}{dx} b \frac{d^2 w}{dx^2} \right]_0^L = 0$$

$$\frac{d}{dx} \left(b \frac{d^2 w}{dx^2} \right) = V \quad (\text{Shear force})$$

$$b \frac{d^2 w}{dx^2} = M \quad (\text{Bending moment})$$

B.C



$$w(0) = \frac{dw(0)}{dx} = 0$$

$$v(0) = \frac{dv(0)}{dx} = 0$$

$$\frac{d}{dx} \left(b \frac{d^2 w}{dx^2} \right)_{x=L} = 0$$

$$\left(b \frac{d^2 w}{dx^2} \right)_{x=L} = M_0$$



Some Examples

Example 2

Step 3

$$\int_0^L \left(b \frac{d^2 v}{dx^2} \frac{d^2 w}{dx^2} - v f \right) dx - \left[\frac{dv}{dx} \right]_{x=L} M_0 = 0$$

$$B(v, w) = \int_0^L \left(b \frac{d^2 v}{dx^2} \frac{d^2 w}{dx^2} \right) dx$$

or $B(v, w) = l(v)$ where

$$l(v) = \int_0^L v f dx + \left[\frac{dv}{dx} \right]_{x=L} M_0$$

Symmetric & Bilinear

Linear

The functional $I(w)$ can be written as:

$$I(w) = \int_0^L \left[\frac{b}{2} \left(\frac{d^2 w}{dx^2} \right)^2 - w f \right] dx - \left[\frac{dw}{dx} \right]_{x=L} M_0$$



Some Examples

Example 3 Steady heat conduction in a two-dimensional domain Ω

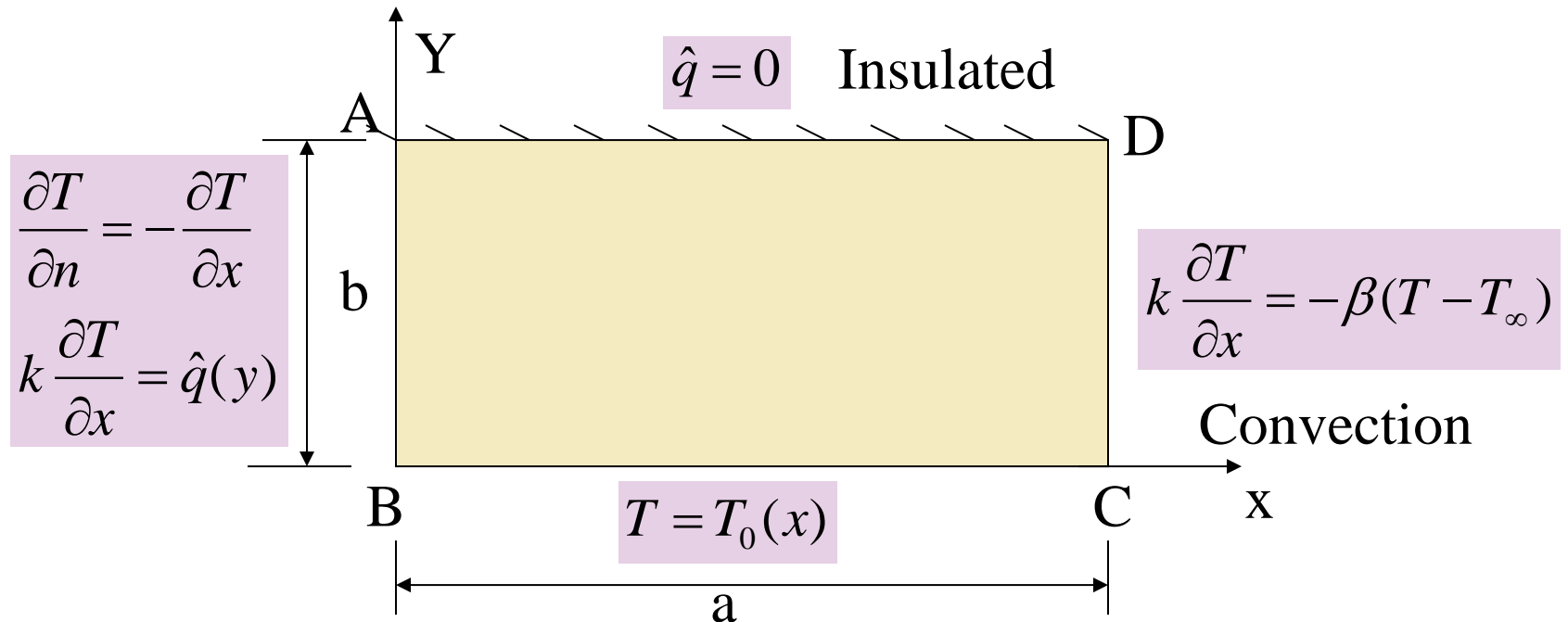
Consider a 2D heat transfer problem

$$-k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right) = q_0 \quad \text{in } \Omega$$

q_0 : uniform heat generation

k : conductivity of the isotropic material

T : temperature





Some Examples

Example 3 Step 1

$$\int_{\Omega} w \left[-k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right) - q_0 \right] dx dy = 0$$

Step 2

$$\int_{\Omega} \left[k \left(\frac{\partial w}{\partial x} \frac{\partial T}{\partial x} + \frac{\partial w}{\partial y} \frac{\partial T}{\partial y} \right) - w q_0 \right] dx dy - \oint_{\Gamma} w k \left(\frac{\partial T}{\partial x} n_x + \frac{\partial T}{\partial y} n_y \right) ds = 0 \quad (*)$$

$$k \left(\frac{\partial T}{\partial x} n_x + \frac{\partial T}{\partial y} n_y \right) = k \frac{\partial T}{\partial n} = q_n$$

T=Primary variable
 q_n =Secondary variable (heat flux)

on $\Gamma_1 = AB$ ($n_x = -1, n_y = 0$) $\Rightarrow \hat{q}(y)$
on $\Gamma_2 = BC$ ($n_x = 0, n_y = -1$) $\Rightarrow T_0(x)$
on $\Gamma_3 = CD$ ($n_x = 1, n_y = 0$) $\Rightarrow k \frac{\partial T}{\partial n} + \beta(T - T_{\infty}) = 0$
on $\Gamma_4 = DA$ ($n_x = 0, n_y = 1$) $\Rightarrow \frac{\partial T}{\partial n} = 0$

Some Examples

Example 3

Step 3

$$\oint_{\Gamma} wk \left(\frac{\partial T}{\partial x} n_x + \frac{\partial T}{\partial y} n_y \right) ds = \oint_{\Gamma} wk \left(\frac{\partial T}{\partial n} \right) ds =$$

$$\oint_{\Gamma_1} wq_n ds + \oint_{\Gamma_2} 0k \left(\frac{\partial T}{\partial n} \right) ds - \oint_{\Gamma_3} w[\beta(T - T_{\infty})] ds + \oint_{\Gamma_4} w(0) ds =$$

$$- \int_0^b w(0, y) \hat{q}(y) dy - \beta \int_0^b w(a, y) [T(a, y) - T_{\infty}] dy$$

w should satisfy the EBC

Substituting in (*) we have

$$\int_{\Omega} \left[k \left(\frac{\partial w}{\partial x} \frac{\partial T}{\partial x} + \frac{\partial w}{\partial y} \frac{\partial T}{\partial y} \right) - wq_0 \right] dx dy + \int_0^b w(0, y) \hat{q}(y) dy + \beta \int_0^b w(a, y) [T(a, y) - T_{\infty}] dy = 0$$

$$B(w, T) = l(w)$$



Some Examples

Example 3

$$B(w, T) = \int_{\Omega} \left[k \left(\frac{\partial w}{\partial x} \frac{\partial T}{\partial x} + \frac{\partial w}{\partial y} \frac{\partial T}{\partial y} \right) \right] dx dy + \beta \int_0^b w(a, y) T(a, y) dy$$

$$l(w) = \int_{\Omega} w q_0 dx dy - \int_0^b w(0, y) \hat{q}(y) dy + \beta \int_0^b w(a, y) T_{\infty} dy$$

The quadratic functional is given by:

$$I(T) = \frac{k}{2} \int_{\Omega} \left[\left(\frac{\partial T}{\partial x} \right)^2 + \left(\frac{\partial T}{\partial y} \right)^2 \right] dx dy - \int_{\Omega} T q_0 dx dy + \int_0^b T(0, y) \hat{q}(y) dy + \beta \int_0^b \frac{1}{2} [T^2(a, y) - 2T(a, y) T_{\infty}] dy$$



Linear and Bilinear Forms

Conclusions

- 1- The weak form of a DE is the same as the statement of the total potential energy.
- 2- Outside solid mechanics $I(u)$ may not have meaning of energy but it is still a use mathematical tools.
- 3- Every DE admits a weighted-integral statement, or a weak form exists for every DE of order two or higher.
- 4- Not every DE admits a functional formulation. For a DE to have a functional formulation, its bilinear form should be symmetric in its argument.
- 5- Variational or FE methods do not require a functional, a weak form of the equation is sufficient.
- 6- If a DE has a functional, the weak form is obtained by taking its first variation.



References

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