دانشگاه صنعتی اصفهان

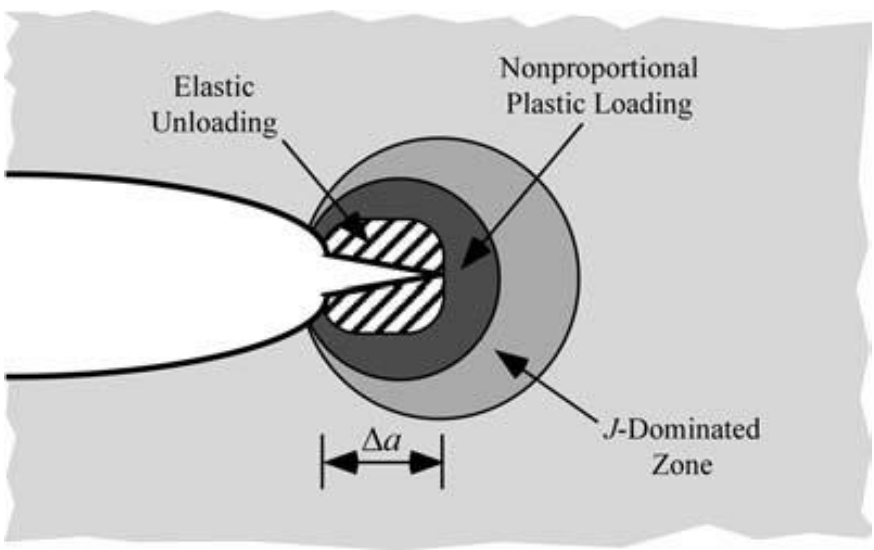
دانشکده مکانیک

Two-Parameter Fracture Mechanics

J-Controlled Crack Growth

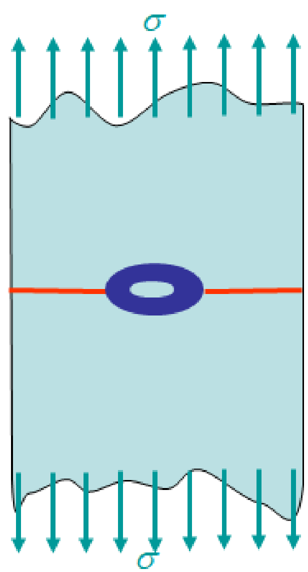
The material directly in front of the crack violates the single-parameter assumption because the loading is highly nonproportional, i.e., the various stress components increase at different rates and some components actually decrease. In order for the crack growth to be J controlled, the elastic unloading and nonproportional plastic loading regions must be embedded within a zone of J dominance. When the crack grows out of the zone of J dominance, the measured R curve is no longer uniquely characterized by J.

In small-scale yielding, there is always a zone of J dominance because the crack-tip conditions are defined by the elastic stress intensity, which depends only on the current values of the load and crack size. The crack never grows out of the J-dominated zone as long as all the specimen boundaries are remote from the crack tip and the plastic zone.

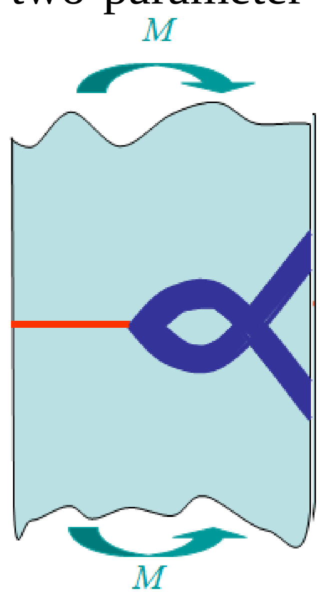


Crack Tip Constraint under Large-Scale Yielding

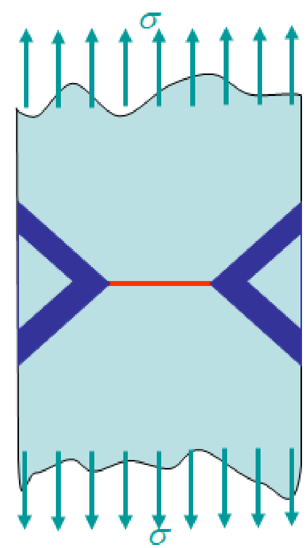
Actually, the plastic strain concentrations depend on the experiment which might be of the forms depicted in following pictures. It appears that the plastic zones are not reproducible from one test to another. Regarding the crack initiation criterion, we can say that the solution is no longer uniquely governed by J. The relation between J and δ_t is dependent on the configuration and on the loading. The critical J_C measured for an experiment might not be valid for another one. A two-parameter characterization is thus required.



Large yielding: two side cracks subjected to uniform tension.



Large yielding: one side crack subjected to a bending moment.



Large yielding: one inner crack subjected to uniform tension.

The Elastic *T* Stress

- Williams showed that the crack tip stress fields in an isotropic elastic material can be expressed as an infinite power series:

$$\sigma_{rr} = \frac{1}{\sqrt{2\pi r}}\left\{\frac{K_I}{4}\left[5\cos\frac{\theta}{2} - \cos\frac{3\theta}{2}\right] + \frac{K_{II}}{4}\left[-5\sin\frac{\theta}{2} + 3\sin\frac{3\theta}{2}\right]\right\} + T\cos^2\theta + O(r^{1/2}) + \ldots$$

$$\sigma_{\theta\theta} = \frac{1}{\sqrt{2\pi r}}\left\{\frac{K_I}{4}\left[3\cos\frac{\theta}{2} + \cos\frac{3\theta}{2}\right] + \frac{K_{II}}{4}\left[-3\sin\frac{\theta}{2} - 3\sin\frac{3\theta}{2}\right]\right\} + T\sin^2\theta + O(r^{1/2}) + \ldots$$

$$\sigma_{r\theta} = \frac{1}{\sqrt{2\pi r}}\left\{\frac{K_I}{4}\left[\sin\frac{\theta}{2} + \sin\frac{3\theta}{2}\right] + \frac{K_{II}}{4}\left[\cos\frac{\theta}{2} + 3\cos\frac{3\theta}{2}\right]\right\} - T\sin\theta\cos\theta + O(r^{1/2}) + \ldots$$

- Although the third and higher terms in the Williams solution, which have positive exponents on *r*, vanish at the crack tip, the second (uniform) term remains finite. It turns out that this second term can have a profound effect on the plastic zone shape and the stresses deep inside the plastic zone.

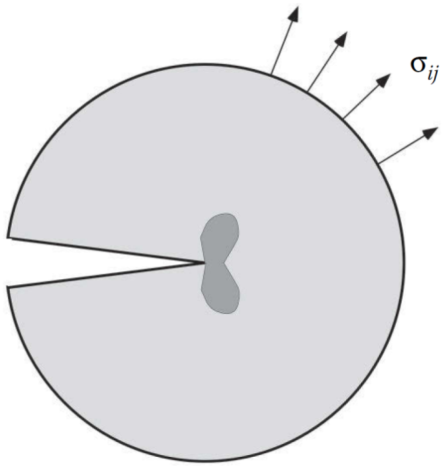
$$\sigma_{ij} = \frac{K_I}{\sqrt{2\pi r}} f_{ij}(\theta) + \begin{bmatrix} T & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \nu T \end{bmatrix}$$

→ plane strain

T is a uniform stress in the *x* direction, which induces a stress *T* in the *z* direction in plane strain.

A modified boundary layer analysis

- The first two terms of the Williams series are applied as boundary conditions:

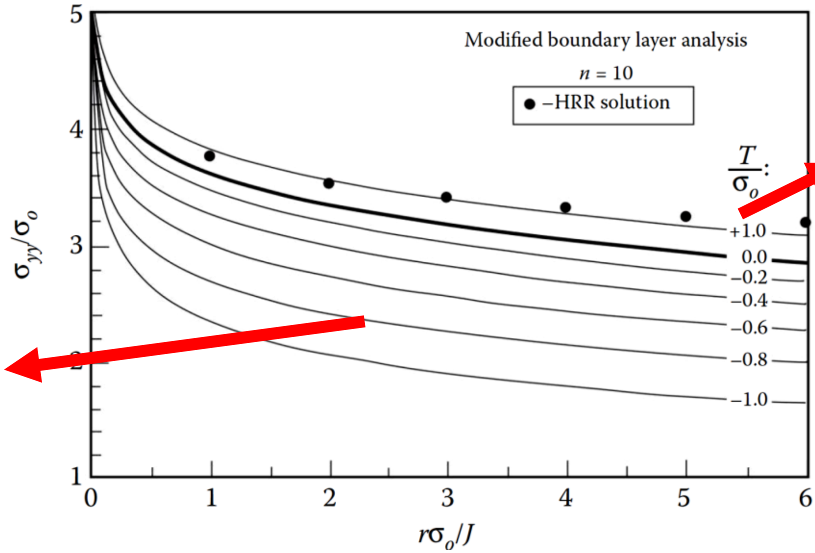


$$\sigma_{ij} = \frac{K_I}{\sqrt{2\pi r}} f_{ij}(\theta) + T\,\delta_{1i}\delta_{1j}$$

- Stress fields obtained from modified boundary layer analysis:

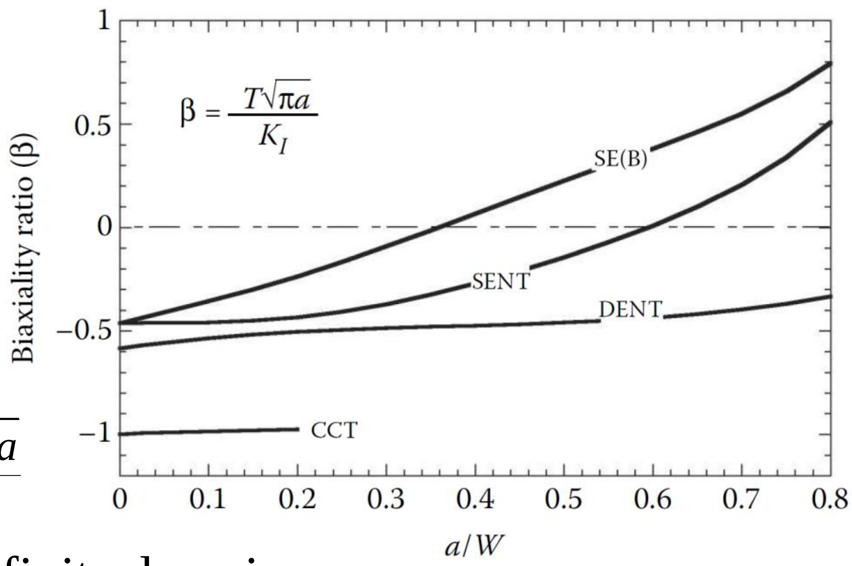
Plastic analysis: σ_{yy} is redistributed!

High negative T stress:
- Decreases σ_{yy}
- Decreases triaxiality



Positive T stress:
- Slightly Increases σ_{yy} and increase triaxiality

T-stress



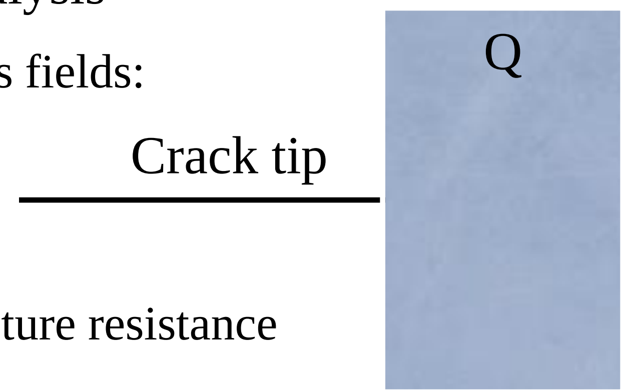
- Higher order terms in stress expansion:
  - *T stress* (linear analysis)
    * Constant σ_{xx} in LEFM expansion.
    * T stress redistributes stress field
    * Nondimensional biaxiality ratio: $\beta = \frac{T\sqrt{\pi a}}{K_I}$
    * for example β = -1 for mode-I crack in infinite domain.
    * β depend on particular geometry/loading configuration
    * Effect of T(β) on toughness:

High (+) T ➡ constrained (triaxial) stress ➡ Toughness ↘ Ductility ↘

Low (-) T ➡ Lose constraint ➡ Toughness ↗ Ductility ↗

* T stress also influences crack path stability (particularly in dynamic fracture)

- ➢ *Q* parameter (*J–Q Theory*) valid for *nonlinear* analysis



- ❖ *A*dded as a *hydrostatic shift* in front of crack to (HRR) stress fields:

$$\sigma_{ij} \approx (\sigma_{ij})_{T=0} + Q\sigma_0\delta_{ij} \qquad \left(|\theta| \le \frac{\pi}{2}\right)$$

- ❖ Similar to T positive Q increases triaxiality and reduces fracture resistance

$$J_c = J_c(Q)$$

High (+) Q ⇨ constrained (triaxial) stress ⇨ Toughness ↘ Ductility ↘

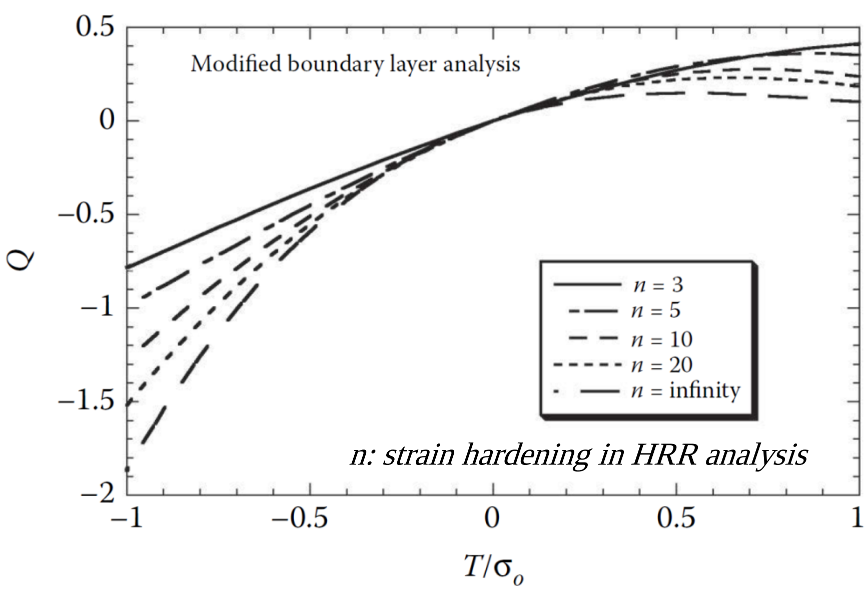
Low (-) Q ⇨ Lose constraint ⇨ Toughness ↗ Ductility ↗

- ➢ *More number of parameters:* with extensive deformation two-parameter models such as *K*, *T* or *J*, *Q* eventually break.

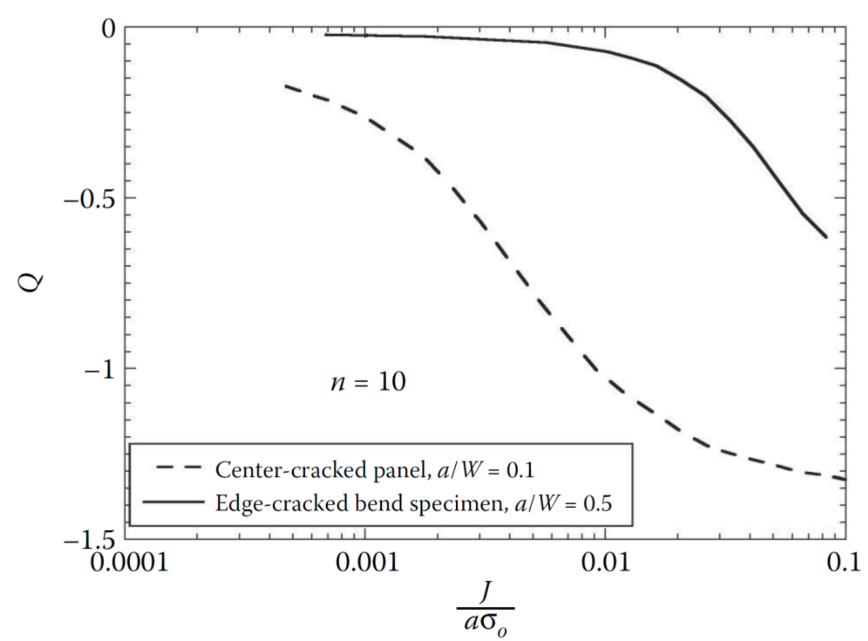
- *Q defined as :*

$$Q \equiv \frac{\sigma_{yy} - (\sigma_{yy})_{T=0}}{\sigma_0} \quad at \quad \theta = 0 \quad \text{and} \quad \frac{r\sigma_0}{J} = 2$$

Referring to Figure *, we see that Q is negative when T is negative.



Relationship between Q and T



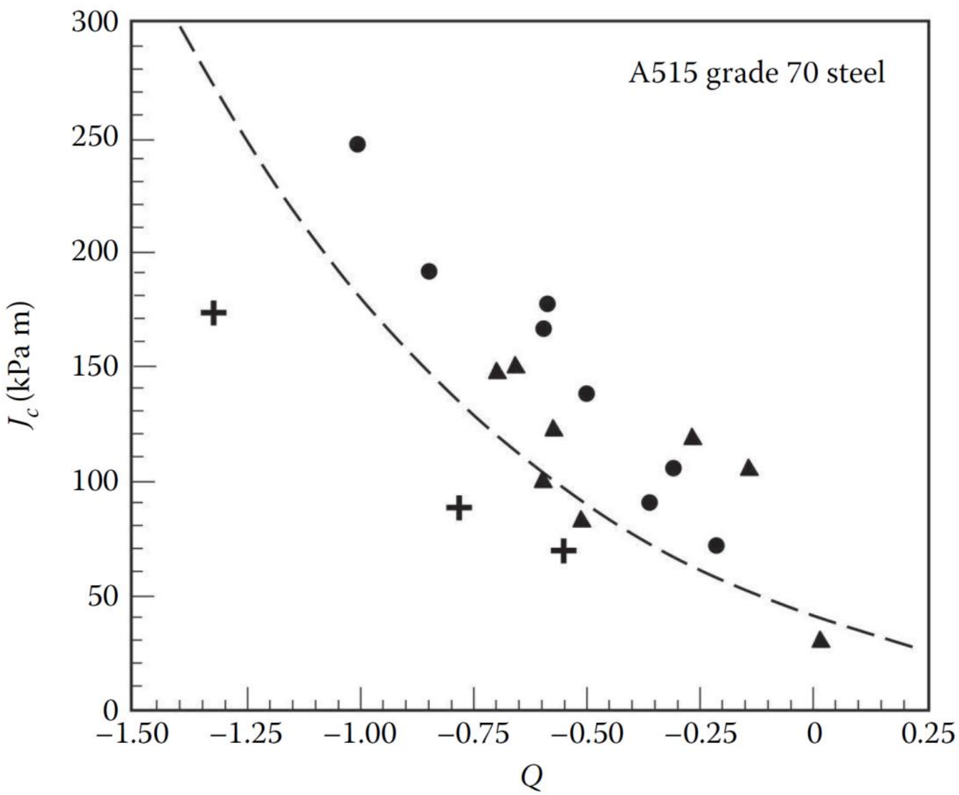
Evolution of the Q parameter with deformation in two geometries

- The *J–Q* Toughness Locus

❖ in *J–Q* theory, an additional degree of freedom has been introduced, which implies that the critical J value for a given material depends on Q:

$$J_c = J_c(Q)$$

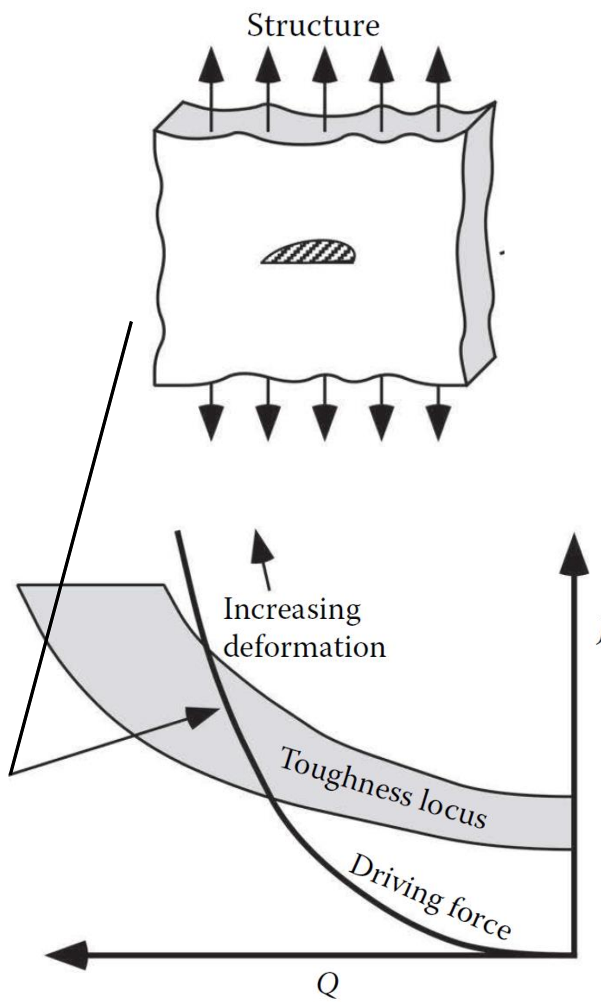
The fracture toughness is no longer viewed as a single value; rather, it is a curve that defines a critical locus of J and Q values.



J–Q toughness locus for SE(B) specimens of A515 Grade 70 steel.

➢ The *J–Q* Toughness Locus

Single-parameter fracture mechanics theory assumes that toughness values obtained from laboratory specimens can be transferred to structural applications. Two-parameter approaches such as *J–Q* theory imply that the laboratory specimen must match the constraint of the structure; that is, the two geometries must have the same *Q* at failure in order for the respective J_c values to be equal. The figure illustrates the application of the *J–Q* approach to structures. The applied *J* versus *Q* curve for the configuration of interest is obtained from finite element analysis and plotted with the *J–Q* toughness locus. Failure is predicted when the driving force curve passes through the toughness locus. Since toughness data are often scattered, however, there is not a single unambiguous cross-over point. Rather, there is a range of possible J_c values for the structure.



Application of a J–Q toughness locus. Failure occurs when the applied J–Q curve passes through the toughness locus.

Limitations of Two-Parameter Fracture Mechanics

The *T* stress approach, *J*–*Q* theory are examples of two-parameter fracture theories, where a second quantity (e.g., *T*, *Q*) has been introduced to characterize the crack tip environment. These approaches assume that the crack tip fields contain two degrees of freedom. When single-parameter fracture mechanics is valid, the crack tip fields have only one degree of freedom. In such cases, any one of several parameters (e.g., *J*, *K*, or CTOD) will suffice to characterize the crack tip conditions, provided the parameter can be defined unambiguously; *K* is a suitable characterizing only when an elastic singularity zone exists ahead of the crack tip. Similarly, the choice of a second parameter in the case of two-parameter theory is mostly arbitrary, but the *T* stress has no physical meaning under large-scale yielding conditions.

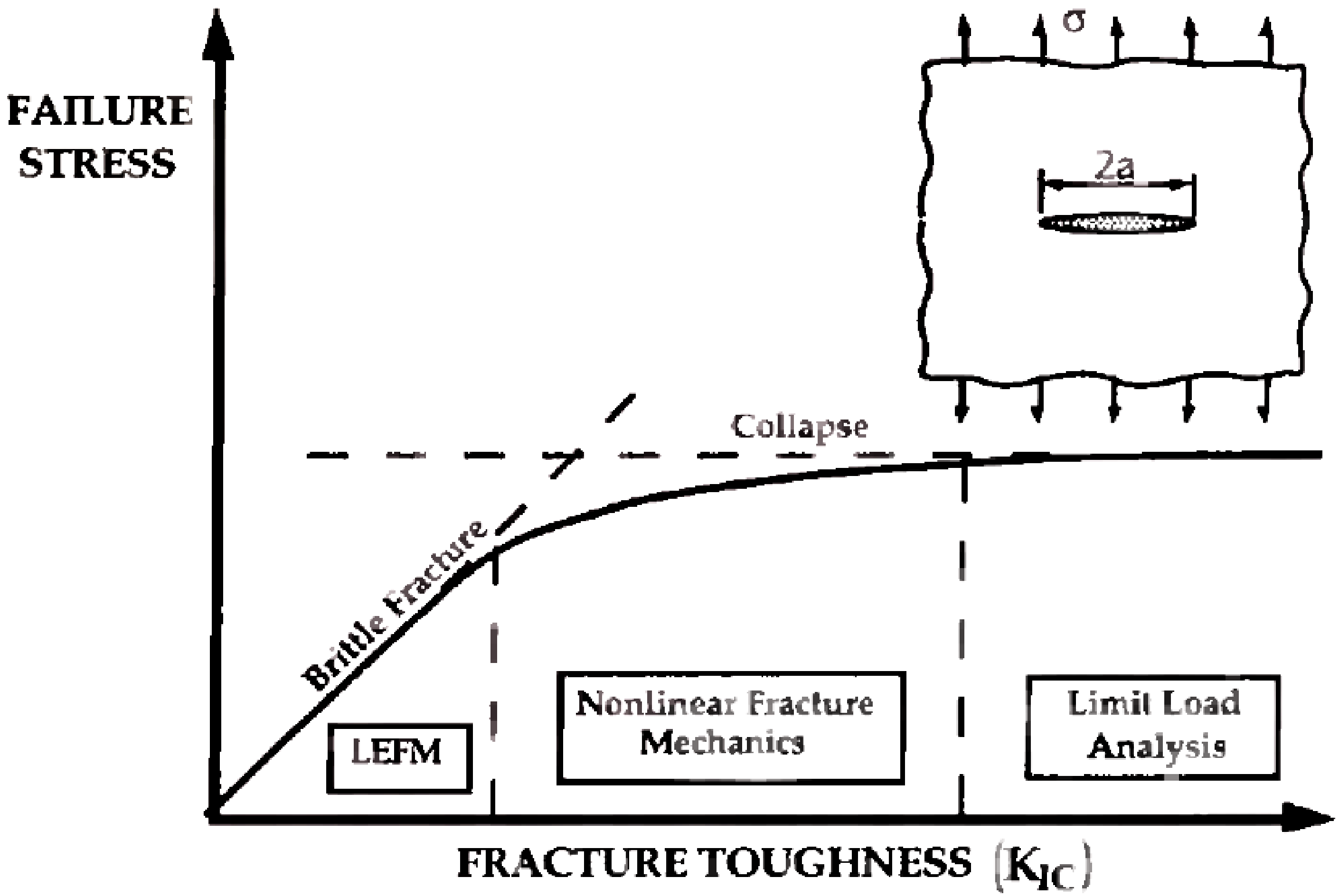
Limitations of Two-Parameter Fracture Mechanics

The characterization of crack tip stress and strain fields is fundamental to fracture mechanics. In elastic–plastic fracture mechanics, it has now been well established the crack tip stress/strain fields in structural components show wide range of variations, and two parameter descriptions have been developed to characterize these stress/strain fields. In this methodology, the first parameter measures the degree of crack-tip deformation, as characterized by J (or equivalently CTOD). The second parameter, characterizes the degree of crack tip constraint, which quantifies the level of deviation of stress/strain fields from HRR fields. The most commonly used second parameters are T-stress, Q-factor and A2-term, corresponding to the J–T, J–Q and J–A2 characterizations. It has been showed that two-parameter approaches provide effective characterization of plane-strain elastic–plastic crack tip fields in a variety of crack configurations and loading conditions.

Limitations of Two-Parameter Fracture Mechanics

- Low-constraint configurations like the center-cracked panel and shallow notched bend specimens diverge from single-parameter theory almost immediately.
- Deeply notched bend specimens maintain high constraint to relatively high J values.
- Low-constraint geometries can be treated with two-parameter theory, and high constraint geometries can be treated with single-parameter theory in many cases. When high constraint geometries violate the single-parameter assumption, however, two-parameter theory is of little value.

Governing fracture mechanism and fracture toughness

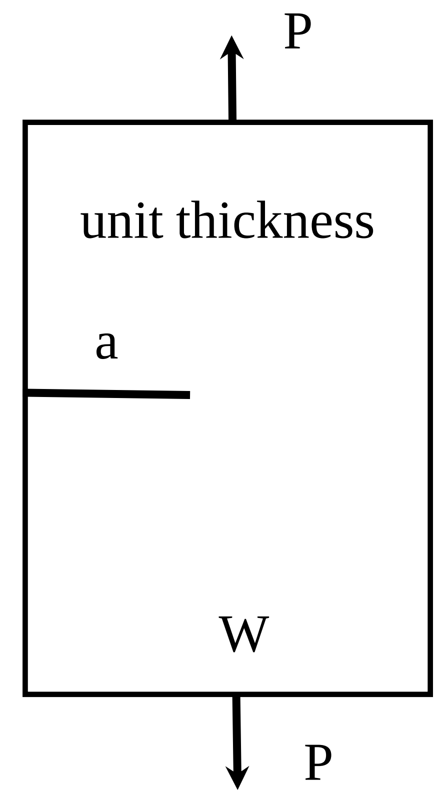


Fracture vs. Plastic collapse

$$\sigma_{\text{net}} = \frac{P}{W-a} = \sigma \frac{W}{W-a}$$

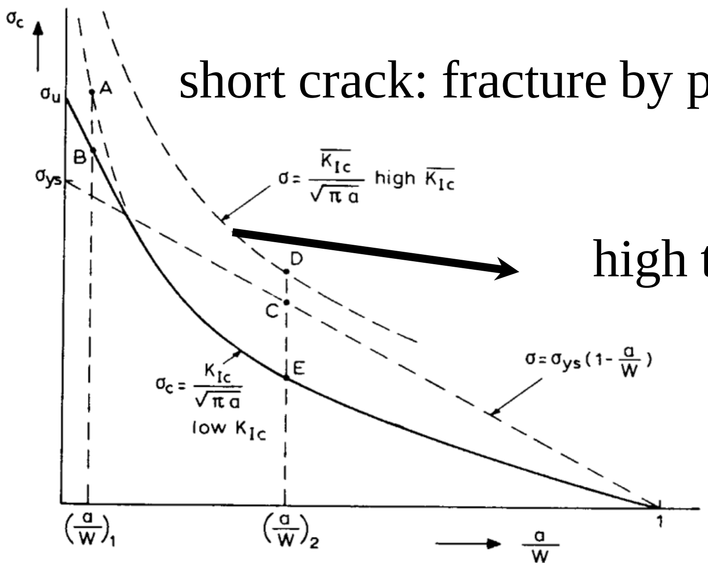
$$\sigma = \frac{P}{W}$$

(cracked section)



Yield: $$\sigma \frac{W}{W-a} = \sigma_{ys} \longrightarrow \sigma = \sigma_{ys}\left(1 - \frac{a}{W}\right)$$

short crack: fracture by plastic collapse!!!



high toughness materials:yielding before fracture

LEFM applies when $\sigma_c \leq 0.66\sigma_{ys}$

Example: Estimate the failure load under uniaxial tension for a center-cracked panel of aluminum alloy of width W=500 mm, and thickness B=4 mm, for the following values of crack length $2a$ = 20 mm and $2a$ = 100 mm. Yield stress σ_y =350 MPa and fracture toughness K_{Ic}=70 MPa m.

Solution: There are two possible failure modes: plastic collapse and brittle fracture. We will assess the load level required for each mode to prevail.

(i) $2a = 20$ mm. Plastic collapse load $F_{pc} = \sigma_{ys} \cdot (W - 2a) \cdot B = 672$ kN

Fracture load $F_c = \sigma_c \cdot W \cdot B$ where $\sigma_c = \dfrac{K_{IC}}{\sqrt{\pi a \sec(\pi a / W)}} = 394.6$ MPa
thus $F_c = 790$ kN.

The actual failure load is the smaller of the above results, 672 kN.

(ii) $2a = 100$ mm. Plastic collapse load $F_{pc} = \sigma_{ys} \cdot (W - 2a) \cdot B = 560$ kN

Fracture load $F_c = \sigma_c \cdot W \cdot B$ where $\sigma_c = \dfrac{K_{IC}}{\sqrt{\pi a \sec(\pi a / W)}} = 172.2$ MPa
thus $F_c = 334.57$ kN.

The actual failure load is the smaller of the above results, 334.57 kN.