

1- The plate structure shown in Figure 1 is loaded and deforms in the plane of the figure. The applied load at  $D$  and the supports at  $I$  and  $N$  extend over a fairly narrow area. Give a list of what you think are the likely “trouble spots” that would require a locally finer finite element mesh to capture high stress gradients. Identify those spots by its letter and a reason.

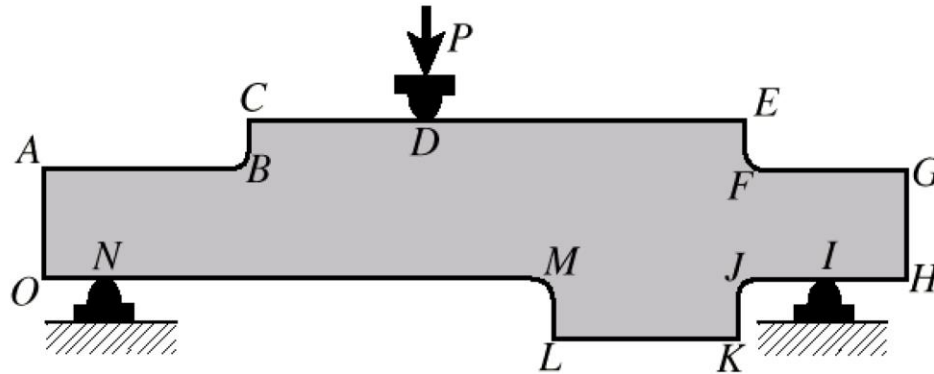
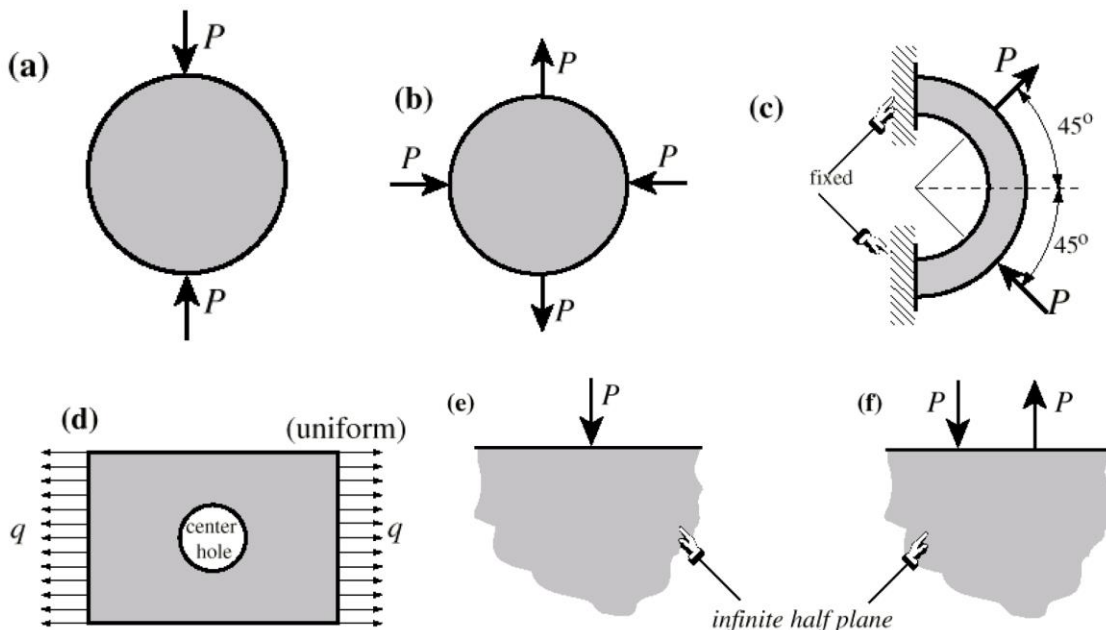


Fig. 1 The plate structure

2- Identify the symmetry and antisymmetry lines in the two-dimensional problems illustrated in Figure 2a-f. Having identified those symmetry/antisymmetry lines, state whether it is possible to cut the complete structure to one half or one quarter before laying out a finite element mesh. Then draw a coarse FE mesh indicating, with rollers or fixed supports, which kind of displacement BCs you would specify on the symmetry or antisymmetry lines.

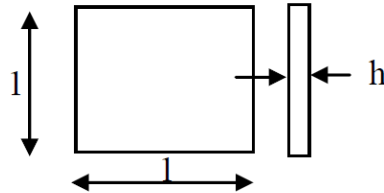


- 3- Consider the square, isotropic, elastic body of thickness  $h$  shown in Figure below. Suppose that the displacement are approximated by:

$$u(x, y) = (1-x)y u_1 + x(1-y) u_2$$

$$v(x, y) = 0$$

Assuming that the body is in the state of the plane stress. Derive 2 by 2 stiffness matrix of the unit square.



- 4- Construct the weak form and, whenever possible, quadratic functional.

- a) *The Timoshenko (shear-deformable) beam theory:*

$$\left. \begin{aligned} -\frac{d}{dx} \left[ GKA \left( \frac{dw}{dx} + \Psi \right) \right] &= f \\ -\frac{d}{dx} \left( EI \frac{d\Psi}{dx} \right) + GKA \left( \frac{dw}{dx} + \Psi \right) &= 0 \end{aligned} \right\} \text{ for } 0 < x < L$$

$$w(0) = w(L) = 0, \quad \left( EI \frac{d\Psi}{dx} \right) \Big|_{x=0} = \left( EI \frac{d\Psi}{dx} \right) \Big|_{x=L} = 0$$

where  $G$ ,  $K$ ,  $A$ ,  $E$ ,  $I$ , and  $f$  are functions of  $x$ .

- b) *The Euler–Bernoulli–von Kármán nonlinear theory of beams:*

$$-\frac{d}{dx} \left\{ a \left[ \frac{du}{dx} + \frac{1}{2} \left( \frac{dw}{dx} \right)^2 \right] \right\} = q \quad \text{for } 0 < x < L$$

$$\frac{d^2}{dx^2} \left( b \frac{d^2 w}{dx^2} \right) - \frac{d}{dx} \left\{ a \frac{dw}{dx} \left[ \frac{du}{dx} + \frac{1}{2} \left( \frac{dw}{dx} \right)^2 \right] \right\} = f$$

$$u = w = 0 \quad \text{at } x = 0, L; \quad \left( \frac{dw}{dx} \right) \Big|_{x=0} = 0; \quad \left( b \frac{d^2 w}{dx^2} \right) \Big|_{x=L} = M_0$$

where  $a$ ,  $b$ ,  $q$ , and  $f$  are functions of  $x$ , and  $M_0$  is a constant. Here  $u$  denotes the axial displacement and  $w$  the transverse deflection of the beam.

- 5- Compute the coefficient matrix and the right-hand side of the  $N$ -parameter Rayleigh–Ritz approximation of the equation

$$-\frac{d}{dx} \left[ (1+x) \frac{du}{dx} \right] = 0 \quad \text{for } 0 < x < 1$$

$$u(0) = 0, \quad u(1) = 1$$

Use algebraic polynomials for the approximation functions. Specialize your result for  $N = 2$  and compute the Ritz coefficients.

*Answer:*  $c_1 = \frac{55}{131}$  and  $c_2 = -\frac{20}{131}$ .

- 6- Solve the Poisson equation governing heat conduction in a square region (see Example 2.6):

$$-k\nabla^2 T = q_0$$

$$T = 0 \quad \text{on sides } x = 1 \text{ and } y = 1$$

$$\frac{\partial T}{\partial n} = 0 \quad (\text{insulated}) \quad \text{on sides } x = 0 \text{ and } y = 0$$

using a one-parameter Rayleigh–Ritz approximation of the form

$$T_1(x, y) = c_1(1-x^2)(1-y^2)$$

*Answer:*  $c_1 = \frac{5q_0}{16k}$ .

- 7- Find a one-parameter approximate solution of the nonlinear equation

$$-2u \frac{d^2 u}{dx^2} + \left( \frac{du}{dx} \right)^2 = 4 \quad \text{for } 0 < x < 1$$

subject to the boundary conditions  $u(0) = 1$  and  $u(1) = 0$ , and compare it with the exact solution  $u_0 = 1 - x^2$ . Use (a) the Galerkin method, (b) the least-squares method, and (c) the Petrov–Galerkin method with weight function  $w = 1$ .

*Answer:* (a)  $(c_1)_1 = 1$ ,  $(c_1)_2 = -2$ .

- 8- Evaluate the following coefficient matrices and source vector using the linear Lagrange interpolation functions:

$$K_{ij}^e = \int_{x_A}^{x_B} (a_0 + a_1 x) \frac{d\psi_i^e}{dx} \frac{d\psi_j^e}{dx} dx$$
$$m_{ij}^e = \int_{x_A}^{x_B} (c_0 + c_1 x) \psi_i^e \psi_j^e dx, \quad f_i^e = \int_{x_A}^{x_B} (q_0 + q_1 x) \psi_i^e dx$$

where  $a_0$ ,  $a_1$ ,  $c_0$ ,  $c_1$ ,  $q_0$ , and  $q_1$  are constants.